# PRODUCT APPROVAL SUPPORTING CALCULATIONS Brickmould Vinyl Double Hung Window

**REPORT TO:** 

JELD-WEN WINDOWS & DOORS 3737 LAKEPORT BLVD KLAMATH FALLS, OREGON

REPORT NUMBER: NCTL-110-23985-1 REPORT DATE: 02/02/21

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#### **Scope**

National Certified Testing Laboratories was contracted by Jeld-Wen Windows & Doors to evaluate alternate installation methods for their Brickmould Vinyl Double Hung windows. The evaluation is based on physical testing and product certifications. Reference standards utilized in this project include:

Florida Building Code, Building. International Code Council.

ANSI/AWC *National Design Specification (NDS) for Wood Construction*. American Wood Council.

AISI S100 North American Specification for the Design of Cold-Formed Steel Structural Members. American Iron and Steel Institute.

ICC-ES Report ESR-1976 *ITW Buildex TEKS Self-Drilling Fasteners*. ICC Evaluation Service.

NOA 16-1222.06 Tapcon Concrete and Masonry Anchors with Advanced Threadform Technology. Miami-Dade County Product Control Section.

The anchorage analyses presented herein do not address the water resistance, water penetration or air infiltration performance of the installation method or the installed product. In addition, the analyses rely on the assumption that the building substrate is capable of withstanding incurred loads.

#### Certification of Independence

In accordance with Rule 61G20-3 Florida Administrative Code, National Certified Testing Laboratories hereby certifies the following:

- National Certified Testing Laboratories does not have, nor does it intend to acquire
  or will it acquire, a financial interest in any company manufacturing or distributing
  products tested or labeled by the agency.
- National Certified Testing Laboratories is not owned, operated or controlled by any company manufacturing or distributing products it tests or labels.
- Joseph A. Reed, P.E. does not have nor will acquire, a financial interest in any company manufacturing or distributing products for which the reports are being issued.
- Joseph A. Reed, P.E does not have, nor will acquire, a financial interest in any other entity involved in the approval process of the product.



#### **Analyses**

#### **Summary of Test Results**

The following table summarizes the various Brickmould Vinyl Double Hung window products and their corresponding performance levels which have been established by testing or product certification.

Table 1 Summary of Test Results

Series/Model	Test Report Number	Size (W x H)	Performance
Brickmould Vinyl Double Hung (Through Frame)	SJW2012-169 (Rev -, 10/02/12)	38" x 74"	+50/-50 psf
Brickmould Vinyl Double Hung (Fin Install)	SJW2012-172 (Rev -, 10/02/12)	38" x 74"	+50/-50 psf
Brickmould Vinyl Double Hung (Through Frame)	SJW2012-173 (Rev -, 10/02/12)	42" x 57"	+50/-50 psf
Brickmould Vinyl Double Hung (Fin Install)	SJW2012-253 (Rev -, 02/01/13)	42" x 57"	+50/-50 psf

Testing documented in Table 1 was conducted by the National Certified Testing Laboratories laboratory in Everett, Washington (Florida Department of Business & Professional Regulation Test Lab No. TST9341, A2LA Certificate 3054.01).

#### **As-Tested Installation Analysis**

For air/water/structural testing the test specimen was secured to a 2x Spruce-Pine-Fir buck. The as-tested installation methods are evaluated on page 4 to page 7. These capacities will be used to prove acceptable alternate anchors and substrates for the windows.

#### **Alternate Anchorages**

Calculations on page 8 through page 10 determine the design capacity of alternate installation anchorages for the window.

#### **Anchorage Requirements**

As-tested spacing must be maintained. It must be determined the anchorages are not overloaded for the approved window size and design pressures. Calculations presented on page 11 show the anchor spacing requirements for the established limiting anchor capacities.

Anchorage requirements established by this report are accurately presented in Drawing D008421.



#### **Attachments**

Appendix A – Revision Log (1 page)



#### As-Tested Installation – Nail Fin to Wood

#8 x 1-1/4" Pan Head Screw

0.062" thick Nail Fin

Spruce-Pine-Fir 2x Wood Substrate Minimum (G=0.42)

Allowable Tension of #8 x 1-1/4" Pan Head Screw

W = 1.6(1.250"-0.062")(82 lb/in) (NDS, Table 12.2B)

W = 156 lb

#### Allowable Pull-Over of #8 x 1-1/4" Pan Head Screw

Validated by Testing

Must maintain anchor spacing and anchor head size

As-tested spacing (48x83): 4" on center

Load to fastener (48x83): (55 psf/144)(48"/2)(4") = 37 lb

As-tested spacing (48x96): 8" on center

Load to fastener (48x96): (35 psf/144)(48"/2)(8") = 47 lb

As-tested anchor head size: 0.314"

**Capacity of Connection is 47 lb** 



#### <u>As-Tested Installation – Through Frame to Wood</u>

#8 Pan Head Screw; 1" penetration to wood

0.060" thick Window Frame

1/4" Maximum Shim Space

Spruce-Pine-Fir 2x Wood Substrate Minimum (G=0.42)

#### Allowable Shear of #8 Pan Head Screw

Z' = 79 lb (See Following 2 Pages)

#### Bending of #8 Pan Head Screw

L = 1/4" (maximum shim space)

 $S = \pi d^3/32 = \pi (0.131)^3/32 = 0.000221 in^3$ 

 $F_b = (1.3)(0.6F_y) = (1.3)(0.6)(90,000 \text{ psi}) = 70,200 \text{ psi} (1.3 \text{ weak axis factor})$ 

 $F_b = M/S = (VL/2)/S (L/2 \text{ for guided bending})$ 

 $V = 2SF_b/L = (2)(0.000221 \text{ in})(70,200 \text{ psi})/0.25" = 124 \text{ lb}.$ 

Capacity of Connection is 79 lb



# <u>As-Tested Installation – Through Frame to Wood</u> (Continued)

# **Lateral Design Strength of Wood Connections**

#### Data

Fastener			
Fastener	=	#8 W	ood Screw
Shank Dia	=	0.164	in.
Root Dia.	=	0.131	in.
$F_{yb}$	=	90,000	psi
Fastener length	=	1.400	in.
Main Memb	er		
Material	=		SPF

Material	=		SPF
G	=	0.42	
θ	=	90	$=$ (Angle of load to grain $0^{\circ} \le \theta \le 90^{\circ}$ )
$F_{e}$	=	3,350	psi
Thickness	=	1.500	in.

#### **Side Member**

Material	=	Vin	yl (PVC)	
G	=	N/A		
θ	=	90	<= (Angle of load	I to grain $0^{\circ} \le \theta \le 90^{\circ}$ )
$F_{es}$	=	13,750	psi	
Thickness	=	0.060	in.	

#### **Calculations**

#### **Lateral Bearing Factors**

D	=	0.131	in.
$\ell_{\rm m}$	=	1.012	in.
$K_{\boldsymbol{\theta}}$	=	1.25	
$K_D$	=	2.20	
$R_{e}$	=	0.244	
$R_{t}$	=	16.87	
$\mathbf{k_1}$	=	1.6013	
$k_2$	=	0.7128	
$k_3$	=	13.20	

<===== Minimum Value



## As-Tested Installation - Through Frame to Wood (Continued)

Yield Mode	$R_d$
$I_{\rm m}$ , $I_{\rm s}$	2.20
II	2.20
III <sub>m</sub> , III <sub>s</sub> , IV	2.20

#### Lateral Design Values, Z

$\begin{array}{cccccccccccccccccccccccccccccccccccc$
Mode II = 79 lbf
$Mode III_m = 97$ lbf
$Mode III_s = 70$ lbf
Mode IV = 99 lbf
$C_D = 1.6$

Wet Service Factor

Fabrication/In-Service  $\frac{\text{Dry/Dry}}{\text{C}_{\text{M}}} = 1.0$ 

In service temperature

mperature  $T \le 100^{\circ}F$   $C_t = 1.0$ 

 $C_g = 1.0$ 

 $C_{\triangle} = 1.0$ 

Is fastener installed in end grain? No

 $C_{eg} = 1.00$  diaphragm? No

Is fastener part of a diaphragm?

 $C_{di} = 1.0$ 

Is fastener toe-nailed? No

 $C_{tn} = 1.00$ 

 $Z' = \frac{79}{}$  lbf



### Alternate Installation - Trough Frame to Steel Stud

#8 Grade 5 Screw

1/4" Maximum Shim Space

Minimum 18 gauge 33 KSI Steel Stud

#### Allowable Shear of #8 Grade 5 Screw

 $P_{ss}/\Omega = 286 \text{ lb } (AAMA TIR A9)$ 

#### Bearing of #8 Grade 5 Screw on Frame

 $F_p = 10,000 \text{ psi}$  D = 0.164" t = 0.060"  $V_a = F_p Dt = (10,000 \text{ psi})(0.164)(0.060) = 98 \text{ lb}$ 

#### Bearing of #8 Grade 5 Screw on Steel Stud

 $V_a = 2.7 DtF_{tu}/3.0$   $V_a = 2.7(0.164")(0.0428")(45,000 psi)/3.0$  $V_a = 284 lb.$ 

#### Tilting of #8 Grade 5 Screw in Steel Stud

 $V_a = 4.2(t_2^3D)^{1/2}F_{tu2}/n_s$   $V_a = 4.2(0.0428"^3 \times 0.164")^{1/2}(45,000 \text{ psi})/3.0$  $V_a = 226 \text{ lb}.$ 

#### Bending of #8 Grade 5 Screw

 $L = 1/4" \text{ (Maximum Shim Space)} \\ S = \pi d^3/32 = \pi (0.116)^3/32 = 0.000153 \text{ in}^3 \\ F_b = (1.3)(0.6F_y) = (1.3)(0.6)(100,000 \text{ psi}) = 78,000 \text{ psi } (1.3 \text{ weak axis factor}) \\ F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)} \\ V = 2SF_b/L = (2)(0.000153 \text{ in}^3)(78,000 \text{ psi})/0.25" = 96 \text{ lb.} \\$ 

**Capacity of Connection is 96 lb.** 



#### Alternate Installation - Through Frame to Concrete

3/16" Tapcon Anchor

2" Minimum Edge Distance, 1-1/4" Minimum Embedment

1/4" Maximum Shim Space

Minimum f'c = 3,000 psi Concrete

#### Allowable Shear of 3/16" Tapcon Anchor

 $P_{ss}/\Omega = 181 \text{ lb}$  (NOA-No. 16-1222.06)

#### Bearing of 3/16" Tapcon Anchor on Frame

 $F_p$  = 10,000 psi D = 0.170" t = (2)(0.080") = 0.160"  $V_a$  =  $F_p$ Dt = (10,000 psi)(0.170")(0.160") = 272 lb

#### Bending of 3/16" Tapcon Anchor

 $L = 1/4" \text{ (Maximum Shim Space)} \\ S = \pi d^3/32 = \pi (0.170")^3/32 = 0.000482 \text{ in}^3 \\ F_b = (1.3)(0.6F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} (1.3 \text{ weak axis factor}) \\ F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)} \\ V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb.} \\ \end{split}$ 

**Capacity of Connection is 181 lb** 



#### Alternate Installation – Through Frame to CMU

3/16" Tapcon Anchor

2" Minimum Edge Distance, 1-1/4" Minimum Embedment

1/4" Maximum Shim Space

Minimum ASTM C90 Concrete Masonry Unit

#### Allowable Shear of 3/16" Tapcon Anchor

 $P_{ss}/\Omega = 135 \text{ lb}$  (NOA-No. 16-1222.06)

#### Bearing of 3/16" Tapcon Anchor on Frame

 $F_p = 10,000 \text{ psi}$  D = 0.170" t = (2)(0.080) = 0.160"  $V_a = F_pDt = (10,000 \text{ psi})(0.170)(0.160) = 272 \text{ lb}$ 

#### Bending of 3/16" Tapcon Anchor

 $L = 1/4" \text{ (Maximum Shim Space)} \\ S = \pi d^3/32 = \pi (0.170")^3/32 = 0.000482 \text{ in}^3 \\ F_b = (1.3)(0.6F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} (1.3 \text{ for weak axis bending)} \\ F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)} \\ V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb.} \\ \\$ 

**Capacity of Connection is 135 lb** 



#### 38x74 +50/-50 psf

#### Anchorage Requirements - Nail Fin

Window Overall Size: 38" x 74"

Window Overall Area:  $(38")(74")/144 = 19.5 \text{ ft}^2$ Window Overall Wind Load:  $(50 \text{ psf})(19.5 \text{ ft}^2) = 975 \text{ lb}$ 

Installed Anchors: 5 head + 5 sill + 2(8) jambs = 26 installed anchors

Minimum Anchor Capacity: 47 lb/anchor

Total Anchor Capacity: (26 anchors)(47 lb/anchor) = 1,222 lb > 975 lb **OK** 

#### **Anchorage Requirements – Through Frame**

Window Overall Size: 38" x 74"

Window Overall Area:  $(38")(74")/144 = 19.5 \text{ ft}^2$ Window Overall Wind Load:  $(50 \text{ psf})(19.5 \text{ ft}^2) = 975 \text{ lb}$ 

Installed Anchors: 3 head + 3 sill + 2(9) jambs = 24 installed anchors

Minimum Anchor Capacity: 79 lb/anchor

Total Anchor Capacity: (24 anchors)(79 lb/anchor) = 1,896 lb > 975 lb **OK** 

#### 42x57 +50/-50 psf

#### Anchorage Requirements - Nail Fin

Window Overall Size: 42" x 57"

Window Overall Area:  $(42")(57")/144 = 16.6 \text{ ft}^2$ Window Overall Wind Load:  $(50 \text{ psf})(16.6 \text{ ft}^2) = 830 \text{ lb}$ 

Installed Anchors: 5 head + 5 sill + 2(6) jambs = 22 installed anchors

Minimum Anchor Capacity: 47 lb/anchor

Total Anchor Capacity: (22 anchors)(47 lb/anchor) = 1,034 lb > 830 lb OK

#### **Anchorage Requirements – Through Frame**

Window Overall Size: 42" x 57"

Window Overall Area:  $(42")(57")/144 = 16.6 \text{ ft}^2$ Window Overall Wind Load:  $(50 \text{ psf})(16.6 \text{ ft}^2) = 830 \text{ lb}$ 

Installed Anchors: 3 head + 3 sill + 2(7) jambs = 20 installed anchors

Minimum Anchor Capacity: 79 lb/anchor

Total Anchor Capacity: (20 anchors)(79 lb/anchor) = 1,580 lb > 830 lb **OK** 



# Appendix A

# Revision Log

<u>Identification</u> <u>Date</u> <u>Page & Revision</u>

Original Issue 02/02/21 Not Applicable